SECTION 500 DRAINAGE REPORT



4561 E. McDowell Road Phoenix, AZ 85008 602.454.0402 602.454.0403 (fax)

To:

Mr. Steve Riley

Project Manager

Subject:

Drainage

Memorandum

Project:

Northern Addition Sidewalks

CDBG Project

AZTEC Project

Number: AZE1212-05

Date: January 21, 2015

46632 SARAH A. SMEDLEY 15

EXPIRES 6/30/2016

From:

Sarah Smedley, PE

Project Engineer

<u>Purpose</u>

The purpose of this technical memorandum is to document the drainage analysis and design of the Northern Addition Sidewalks CDBG Project. There are two main drainage concerns when constructing sidewalk improvements in older subdivisions, street conveyance and adjacent finished floor elevations. Both have been analyzed and the results are presented in this memorandum. A drainage area map and drainage calculations have also been included. Design methodology, criteria and calculations are based on the City of Buckeye's *Storm Water Drainage System Design Manual*.

Existing Conditions

The project is located in the City of Buckeye, Arizona in an area located just north of downtown Buckeye. The subdivision, referred to as the "Northern Addition Plat of Buckeye", was platted in 1929. The project limits include four local streets: Narramore Avenue, Nelson Avenue, Eason Avenue and Edison Avenue between 2nd Street and 4th Street. Edison Avenue is a bid alternate. Currently, these east-west streets have varying widths of pavement with no curb, gutter or sidewalk. The north-south streets in the project limits are recently improved and have curb, gutter and sidewalks. At the intersections with Nelson, Eason and Edison, valley gutters have been constructed to convey street flows to the south.

The overall drainage pattern in the project vicinity is from northwest to southeast. The project streets generally slope to the east. Nelson Avenue, Eason Avenue and Edison Avenue flow east to the north-south streets and the pavement drainage is conveyed south in the existing valley gutters. Narramore from 1st Street to 2nd Street has a one-way crown to the south. There is recently constructed curb and gutter on the south side of Narramore. Flows are conveyed in the existing gutter east to 2nd Street and then south at the intersection. From 2nd Street to 4th Street, the south side of the street flows east to the nearest north-south street and continues south. The north half, however should drain to 4th Street but has pockets of ponding areas, which will be improved through pavement replacement with this project.

During a site visit in July 2014, it was noted that a majority of the homes in the project limits are flood irrigated, with higher finished floors and depressed yards. It was apparent that most of the homes on the south side of the streets are not graded toward the adjacent street as would be done in newer subdivisions, but continue to follow the natural grade of the land.

Floodplain Classification

The Federal Emergency Management Agency (FEMA) has developed Flood Insurance Rate Maps (FIRM) within the project site. The project is located in panel 2580, Map No. 04013C2580L for Maricopa County, Arizona and Incorporated Areas, revised October 16, 2013. The latest FIRM panel for the project has been included with this memorandum as Exhibit 1. The project site is within the FEMA Flood Zone X (Shaded). Zone X (Shaded) is defined as: "Areas of 0.2% annual chance flood; areas of 1% annual chance flood with average depths less than one foot or with drainage areas less than one square mile; and areas protected by levees from 1% annual chance flood."

Proposed Improvements

The proposed pedestrian improvements include the installation of new curb, gutter and sidewalk on both the north and south sides of Narramore between 2nd Street and 4th Street, Eason and Nelson from 3rd to 4th Streets and Edison from 2rd to 4th Streets. Only south curb improvements are proposed for Eason from 2nd Street to 3rd Street, since the north side of the street has new improvements. The proposed curb along the north side of Narramore will extend west past 2nd Street to tie into existing grades without creating an area of ponding at the new curb. With the exception of Edison, all of the streets will now be 32' from back of curb to back of curb, symmetrical about the centerline. Edison, because of existing overhead power lines is shifted 2' to the south between 2nd and 3rd Streets. Edison between 3rd and 4th Streets will be 31' wide, 15' from centerline to the south back of curb, because of the overhead power lines. Concrete driveways, on-street parking with valley gutters and ADA pedestrian ramps will be constructed within the project limits as well. Based on the drainage analysis discussed below, drainage criteria can be met by the construction of either 4-inch or 6inch vertical curb and gutter and areas of pavement replacement. No other drainage improvements are required.

Street Conveyance

A hydrologic study was performed using the Rational Method and NOAA 14 intensity rates to calculate peak flows at all intersections including offsite flows from north of Narramore. The offsite drainage boundary is the canal just north of Narramore. A Drainage Area Map has been included with this memorandum to present the delineation of the drainage areas. As mentioned above, the project generally slopes from northwest to southeast. Drainage areas include the north block and the adjacent street to determine the flow depths. The results of the hydrologic calculations are included.

The pavement hydraulic calculations were performed to determine the depth of flow at each intersection in the project. Depending on the depth of flow, 4-inch vertical curb, 6-

inch vertical curb or additional drainage improvements are recommended. Average existing longitudinal slopes were used for the analysis.

For Nelson, Eason and Edison, the existing cross slope is fairly flat without a pronounced crown. It was assumed that the peak flows would enter the street and flow equally between the north and south curb line. These three streets have existing valley gutters at each north-south intersection which convey the flows south. Therefore, the peak flows for each block are not additive and are analyzed separately.

Narramore does not have valley gutters and was analyzed differently than the other streets. The existing cross slope of Narramore from 1st to 2nd is one way to the south. Although limited improvements are proposed in this section of Narramore, an analysis was provided to show that the flows will not continue past 2nd Street. Flows in the south curb line will not cross the intersection but continue south in 2nd Street. The one-way crown in Narramore transitions to a normal crown after 2nd Street. It was assumed that the peak flows enter the street and flow equally between the north and south curb line. Due to the existing grades along Narramore from 2nd Street to 4th Street, a constant grade would force the gutter line on the north to be much higher than the south gutter line. To avoid a one-way crown between 2nd and 3rd Streets, a north-south valley gutter will be constructed at 3rd Street. Pavement replacement is proposed at this intersection to ensure it drains properly. Narramore from 2nd Street to 3rd Street will drain east to 3rd Street then drain south in 3rd Street at the valley gutter. Narramore from 3rd Street to 4th Street will drain east to 4th Street then south at 4th Street.

An existing church parking lot at the southwest corner of Narramore and 3rd Street currently accepts flows from Narramore into an existing grate catch basin in the center of the parking lot. The new curb and gutter alignment will now contain the flow in Narramore to 3rd Street, bypassing the parking lot. A hydraulic calculation was performed for 3rd Street to verify that the additional flows are contained within the section. The results show that the flows are contained with a flow depth of 4-inches.

Finished Floor Elevations

When new subdivisions are designed, finished floor elevations are typically built 14-inches above the low top of curb to ensure positive drainage to adjacent streets. A concern with installing curb, gutter and sidewalks in older subdivisions, such as Northern Addition, occurs if the proposed curb is higher than the adjacent finished floors, potentially creating ponding and flooding issues. AZTEC surveyed each finished floor elevation within the project boundary. Although the finished floors were not high enough to meet current standards and requirements, all of the houses and businesses on the north side of each street are higher than the proposed top of curb. On the south side, all but two of the homes and businesses are higher as well. On Eason, APN 400-20-055, the finished floor elevation is at the same elevation as the low top of curb. In this location, the existing edge of pavement is only 0.01' lower than the proposed top of curb. This is an existing problem and the proposed improvements are not making the condition worse. The other home is on the south side of Edison between 2nd Street and

3rd Street and has a finished floor elevation at the same elevation as the low top of curb. It is located at the southwest corner of the 3rd Street intersection, APN 400-20-048. Fortunately, this home fronts Roosevelt and the lot drains to the south to Roosevelt. The new curb on Edison will reduce runoff to this lot, thereby improving the lot's drainage conditions. There are also a few homes where a finished floor elevation was not obtained. They were not obtained because these homes fronted Roosevelt or the north-south streets and do not drain to Edison.

Conclusion

Based on the results of the hydraulic calculations it was determined that the streets provide adequate hydraulic capacity to convey the runoff to the north-south streets with no additional drainage improvements, such as curb inlets, retention basins or storm drain. All of the streets have the necessary capacity to convey the peak flows using 4-inch vertical curb except for Narramore between 2nd and 3rd Street. This will require 6-inch vertical curb along the south curb line and 4-inch curb on the north side to convey the 10-year flows without overtopping. The hydraulic calculations are included in this memorandum.

The results of the comparison between the existing finished floor elevations and the proposed top of curb elevations indicate that this project will not create any adverse impacts on the existing neighborhood. Storm water runoff will still drain away from structures and into the adjacent streets. These improvements will not have a negative impact on the flood irrigated properties as well.

Attachments

- FEMA FIRM Panel
- Drainage Area Map
- Hydrology Calculations
- Hydraulic Calculations
- Sidewalk Plans with Finished Floor Elevations



4561 E. McDowell Road Phoenix, AZ 85008 602.454.0402 602.454.0403 (fax)

Exhibits

- 1. FEMA FIRM Panel
- 2. Drainage Area Map

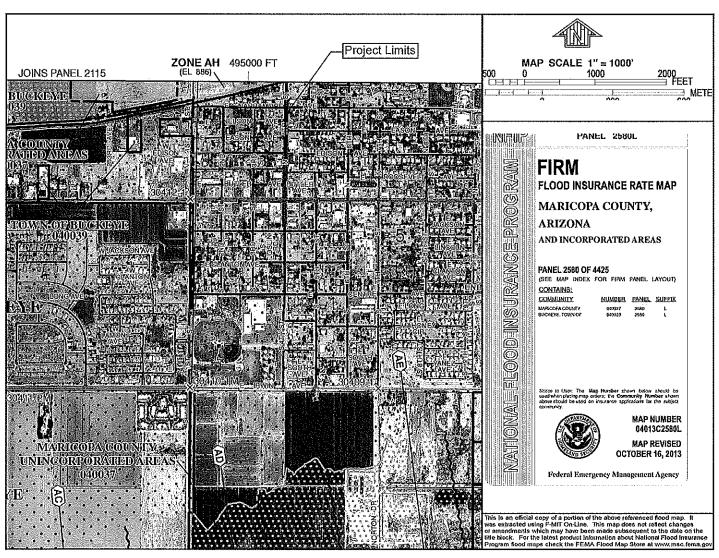
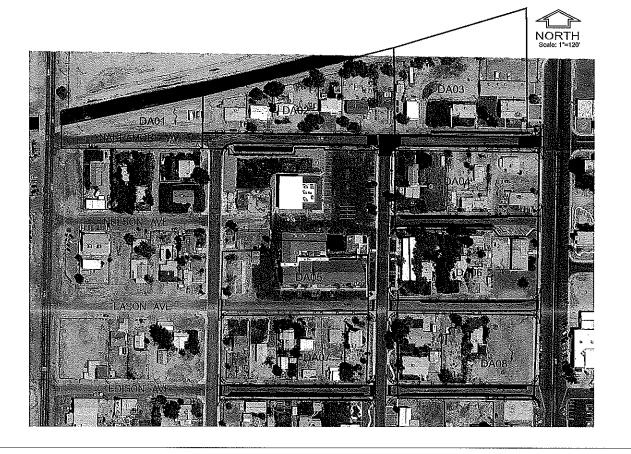


Exhibit 1: FEMA FIRM Panel





LEGEND

DA63

DRAINAGE AREA IO DRAINAGE AREA BOUNDARY

CITY OF BUCKEYE, ARIZONA
STREET TRANSPORTATION DEPARTMENT
HORTHERN ADDITION SIDEWALKS COBG
EXHBIT 2: DRAIHAGE AREA MAP
AZEL12-05

EXSTANCE SOSSON COMPANY
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Hydrology Calculations



Precipitation FCDMC Isopluvial Maps & NOAA ATLAS 14

| Project: | Northern Addition Sidewalks CDBG Project | By: | Sarah Smedley | |
|----------|--|------------|---------------|--|
| Client: | City of Buckeye | Date: | 8/20/2014 | |
| | | Project #: | AZE1212-05 | |

RAINFALL DEPTH-DURATION-FREQUENCY SITE SPECIFIC D-D-F TABLE

| | | | | | Rainfall Dep | oth (inches) | | | - " | |
|-----------|-------|--------|--------|--------|--------------|--------------|--------|--------|---------|---------|
| Frequency | | | | | Dura | ation | | | | |
| (N-year) | 5-min | 10-min | 15-min | 30-min | 1-hour | 2-hour | 3-hour | 6-hour | 12-hour | 24-hour |
| 2 | 0.26 | 0.40 | 0.49 | 0.67 | 0.82 | 0.91 | 0.95 | 1.10 | 1.19 | 1.50 |
| 5 | 0,36 | 0.55 | 0.68 | 0.91 | 1.13 | 1.23 | 1.27 | 1.43 | 1.54 | 1.95 |
| 10 | 0.43 | 0.65 | 0.81 | 1.09 | 1.35 | 1.48 | 1.52 | 1.70 | 1.82 | 2.30 |
| 25 | 0.53 | 08,0 | 0.99 | 1.33 | 1.65 | 1.81 | 1.88 | 2.07 | 2.20 | 2.79 |
| 50 | 0.60 | 0.91 | 1.13 | 1.52 | 1.88 | 2.07 | 2.16 | 2.36 | 2.49 | 3.18 |
| 100 | 0.67 | 1,02 | 1.26 | 1.70 | 2.11 | 2.34 | 2.46 | 2.67 | 2.80 | 3,59 |
| 500 | 0,84 | 1,28 | 1.58 | 2.13 | 2.64 | 2.98 | 3.23 | 3.45 | 3.55 | 4.59 |

| | | | | Ra | infall Intensi | ty (inches/ho | ur) | | | |
|-----------|-------|--------|--------|--------|----------------|---------------|--------|--------|---------|---------|
| Frequency | | | | | Dura | ation | | | | |
| (N-year) | 5-min | 10-min | 15-min | 30-min | 1-hour | 2-hour | 3-hour | 6-hour | 12-hour | 24-hour |
| 2 | 3.14 | 2.39 | 1.98 | 1.33 | 0,82 | 0.45 | 0.32 | 0.18 | 0.10 | 0.06 |
| 5 | 4.30 | 3,27 | 2.70 | 1.82 | 1.13 | 0.62 | 0.42 | 0.24 | 0.13 | 0,08 |
| 10 | 5.16 | 3.92 | 3.24 | 2.18 | 1.35 | 0.74 | 0.51 | 0.28 | 0.15 | 0.10 |
| 25 | 6.30 | 4.79 | 3.96 | 2.66 | 1.65 | 0.91 | 0.63 | 0.35 | 0.18 | 0.12 |
| 50 | 7.16 | 5.45 | 4.52 | 3.04 | 1.88 | 1.04 | 0.72 | 0.39 | 0.21 | 0.13 |
| 100 | 8.03 | 6.12 | 5.04 | 3.40 | 2.11 | 1.17 | 0.82 | 0.45 | 0.23 | 0.15 |
| 500 | 10.06 | 7.68 | 6.32 | 4.26 | 2.64 | 1.49 | 1.08 | 0,58 | 0,30 | 0.19 |

| Project Name: Subject: Location: | Northern Addition Sidev 10-Yr & 100-Yr Peak Dis Buckeye, AZ | - | Date: Computed By: Checked By: | 1/19/2015 SAS TAB | AZTEC (Q) |
|---|---|--|--------------------------------------|--|--|
| Drainage Basin: DA | 01 | - The state of the | | | |
| | | | | | |
| | | | | | |
| | Length of Longest Flowpath = | 0.07 miles | | | |
| | Upper Elevation= Lower Elevation= | | | | |
| | Slope of Longest Flowpath = Kb = | 64.65 ft/mi | | | |
| A #0 | | U.U4UJ | | | |
| Tc=11.4L ^{0.50} K _b ^{0.52} S | 0.31-0.38 | | Q=CIA | | |
| Trials 10-Yea | | | | C _{10 Subdivision} | |
| Tc (min) I(in/ | Calculated hr) Tc (min) | | | C _{10 Paved} C _{10 Composite} | |
| 7 4.6 | | | | | = 3.92 in/hr |
| 8 4.4 | | | | Area _{Subdivision} : | = 0.57 acres |
| 9 4.1 | | | | Area _{Paved} | |
| 10 3.9 | | ок | | Total Area | = 0.84 acres |
| *Minimum Tc = 10 n | nin | | | | |
| Denote | s information that needs to be en | ered. | | 10-Year Storm Event | = <u>2.3</u> cfs |
| Tc=11.4L ^{0,50} K _b ^{0,52} S | 0.31 -0.38 | | Q=CIA | | |
| Trials 100-Ye | ar Event | | | C | = 0.60 |
| 111ais 100-16 | ar Everit Calculated | | | C ₁₀₀ Subdivision C ₁₀₀ Paved | |
| To (min) I (in/ | | | | C _{100 Composite} | EXCENSES AND PROPERTY OF THE P |
| 7.2 | , | | |]: | = 6.12 in/hr |
| 8 6.8 | | | | Area _{Subdivision} | |
| 9 6.9 | | ок | | Area _{Paved} Total Area | |
| *Minimum Tc = 10 n | | OK. | | Total Alea | - 0,04 acres |
| Denote | s information that needs to be en | tered. | 1 | 100-Year Storm Event | = <u>3.7</u> cfs |

| Project Name: Subject: Location: | Northern Addition Sidewall 10-Yr & 100-Yr Peak Discha Buckeye, AZ | | Date: Computed By: Checked By: | 1/19/2015 SAS TAB | RZTEC (D) |
|---|---|--|--------------------------------------|--|--|
| Drainage Basin: DA0 | 02 | | | | |
| | Length of Longest Flowpath = Upper Elevation= Lower Elevation= Slope of Longest Flowpath = Kb = | 509 feet 0.10 miles 884.50 feet 870.70 feet 143.26 ft/mi 0.0376 | | | |
| Tc=11.4L ^{0.50} K _b ^{0.52} Տ ⁻ | 0.31 -0.38 | | Q=CIA | | |
| Trials 10-Year Tc (min) (in/ 7 4.6 8 4.4 9 4.1 10 3.9 *Minimum Tc = 10 m | Calculated (hr) Tc (min) 67 4.6 42 4.7 47 4.8 62 4.9 | ок | | C ₁₀ subdivision [*] C ₁₀ Paved [*] C ₁₀ composite [*] [: Area _{Subdivision} [*] Area _{Paved} [*] Total Area | = 0.95 = 0.66 = 3.92 in/hr = 1.98 acres = 0.40 acres |
| Denotes | s information that needs to be entere | d. | | 10-Year Storm Event | =6.2 cfs |
| Tc=11.4L ^{0.50} K _b ^{0.52} S | 0.310.38 | · · · · | Q=CIA | | |
| Trials 100-Yes Tc (min) I(in/ 7 7.2 8 6.8 9 6.8 10 6.1 *Minimum Tc = 10 m | 3.9 38 4.0 50 4.1 12 4.2 | ОК | | C ₁₀₀ subdivision C ₁₀₀ Paved C ₁₀₀ composite I: Area _{Subdivision} Area _{Paved} Total Area | = 0.95 = 0.66 = 6.12 in/hr = 1.98 acres = 0.40 acres |
| | s information that needs to be entere | d. | 1 | 00-Year Storm Event | = <u>9.6</u> cfs |

| Project Name: Subject: Location: | Northern Addition Sidew 10-Yr & 100-Yr Peak Disc Buckeye, AZ | - | Date: Computed By: Checked By: | 1/19/2015 SAS TAB | PZTEC®) |
|--|--|------------------------|--------------------------------------|-------------------------------|--|
| Drainage Basin: DA03 | 3 | | | | |
| | | | | | |
| | | | | | |
| | Length of Longest Flowpath = | 581 feet 0,11 miles | | | |
| | Upper Elevation= | 884:00 feet | | | |
| | Lower Elevation= | 878.50 feet | | | |
| | Slope of Longest Flowpath = Kb = | 49.97 ft/mi 0.0374 | | | |
| | | | | | |
| Tc=11.4L ^{0.50} K _b ^{0.52} S ^{-0.} | 31-0.38 | | Q=CIA | | |
| Trials 10-Year | Event | | | C _{10 Subdivision} | = 0,60 |
| To rear | Calculated | | | C _{10 Paved} : | |
| Tc (min) l(in/h | r) Tc (min) | | | C _{10 Composite} | KIII SANTAN KANTAN KANT |
| 7 4.67 | 7 6.8 | | | 1: | Service de militare de la companya del companya de la companya del companya de la |
| 8 4.42 | | | | Area Subdivision | = 2.30 acres |
| 9 4.17 | | | | Area _{Paved} | |
| 10 3,92 | | ок | | Total Area | = 2.60 acres |
| *Minimum Tc = 10 mi | п | | | | |
| Denotes | information that needs to be ent | ered. | | 10-Year Storm Event | = <u>6.5</u> cfs |
| | | | | | |
| Tc=11.4L ^{0.59} K _b ^{0.52} S ^{-0.} | 31 _[-0.38 | | Q=CIA | | |
| Trials 100-Year | r Event | | | C _{100 Subdivision} | 0,60 |
| | Calculated | | | C _{100 Paved} | |
| Tc (min) I(in/h | • • • | | | C _{100 Composite} : | |
| 7 7.26 | | | | ļ: - | ACCURATION AND ADDRESS AND ADD |
| 8 6.88 | | | | Area _{Subdivision} : | |
| 9 6.50 10 6.12 | | OK | | Area _{Paved} : | |
| 10 6.12 *Minimum Tc = 10 mi | | OK | | Total Area | = 2.60 acres |
| 101111 | •• | | | | |
| Denotes | information that needs to be ent | ered. | 10 | 00-Year Storm Event | = <u>10.2</u> cfs |
| | | | 1 | | |

| Project Name: Subject: Location: | Northern Addition Sic 10-Yr & 100-Yr Peak I Buckeye, AZ | • | Date: Computed By: Checked By: | 1/19/2015 SAS TAB | AZTEC® |
|--|---|----------------------------|--------------------------------------|--|--|
| Drainage Basin: D |)A04 | | | | |
| | | | | | |
| | | | | | |
| | Length of Longest Flowpati | n = 510 feet 0.10 miles | | | |
| | Upper Elevatio Lower Elevatio | | | | |
| | Slope of Longest Flowpati | n = 22.80 ft/mi | | | |
| | KI | 0.0384 | | | 0.100110.011 |
| Tc=11.4L ^{0.50} K _b ^{0.52} | S ^{-0.31} I ^{-0.38} | | Q=CIA | | |
| Trials 10-Ye | ear Event | | | C _{to Subdivision} = | 0.60 |
| | Calculated | | | C _{16 Paved} = | 0.95 |
| Mount Strengton comments are not | in/hr) Tc (min) | | | C _{10 Composite} = | |
| TOTAL PLANTAGE AND STREET | 4.67 8.2 4.42 8.4 | | | I= Area = | O.O. IIII |
| | 4.42 8.4 4.17 8.6 | | | Area _{Subdivislon} ≐ Area _{Paved} = | UNISCHMUNG PARKET COMPANY COMP |
| A7020 F9078 S0099 (F5676 H | 3.92 8.8 | ок | | Total Area= | |
| Minimum Tc = 10 |) min | | | | |
| Deno | tes information that needs to be | entered. | 1 | i0-Year Storm Event≃ | : 4.6 cfs |
| Tc=11.4L ^{0,50} K _b ^{0,52} | °S ^{-0.31} I ^{-0,38} | | Q=CIA | | |
| Trials 100-\ | /ear Event | | | C _{100 Subdivision} = | = 0.60 |
| | Calculated | | | C _{100 Paved} = | (1):F0295200(F):F43F4F00296(F):F09F0058020600(C) |
| - Charles - Char | in/hr) Tc (min) | | | C _{100 Composite} = | 0.65 |
| | 7.26 7.0 | | |]= | On the control of the |
| | 6.88 7.1 | | | Area _{Subdivision} = | 1.52 acres |
| | 6.50 7.3 6.12 7.4 | ок | | Area _{Paved} ≃ Total Area= | |
| 'Minimum Tc = 10 | | O.K | | rotal Alba- | 1.70 00103 |
| Deno | tes information that needs to be | entered. | 10 | 00-Year Storm Event= | - 7,2 cfs |

| Project Name: Subject: Location: | Northern Addition Sid 10-Yr & 100-Yr Peak D Buckeye, AZ | | Date: Computed By: Checked By: | 1/19/2015 SAS TAB | AZTEC® |
|--|---|----------------------------------|--------------------------------------|---|------------------------------|
| Drainage Basin: D/ | A 05 | | | | |
| | | | | | |
| | Length of Longest Flowpath | = 461 feet 0.09 miles | , | | |
| | Upper Elevation Lower Elevation Slope of Longest Flowpath | n= 878.00 feet n= 876.90 feet | • | | |
| | Kb | | | | . |
| Tc=11.4L ^{0,50} K _b ^{0,52} § | 5 ^{-8,31} [- ^{0,38} | | Q=CIA | | |
| Tc (min) I (ii | ar Event Calculated n/hr) Tc (min) | | | $ m C_{10~Subdivision}$ $ m C_{10~Paved}$ $ m C_{10~Composite}$ | = 0.95 = 0.89 |
| 8 4 9 4 | .67 9.5 .42 9.7 .17 9.9 .92 10.1 | ок | | l: Area _{Subdivision} Area _{Paved} : Total Area: | = 0,27 acres = 1,25 acres |
| *Minimum Tc = 10 | min es information that needs to be e | entered. | | 10-Year Storm Event | =5.3 cfs |
| Tc=11.4L ^{0.50} K _b ^{0.52} \$ | 3 ^{-0.31} l ^{-0.38} | | Q=CIA | | |
| Trials 100-Y | ear Event | | | C ₁₀₀ subdivision | |
| กระคยอยกรักษาการครั้งของส | Calculated n/hr) Tc (min) .26 8.0 | | | C _{100 Paved} C _{100 Composite} ;]: | = 0.89 |
| 8 6 9 6 | .88 8.2 .50 8.4 | O.K | : | Area _{Subdivision} Area _{Paved} | = 1.25 acres |
| 10 6 *Minimum Tc = 10 | .12 8.6 min | OK | | Total Area | = 1.52 acres |
| Denot | es information that needs to be ϵ | ntered. | 1 | 00-Year Storm Event | =8.3 cfs |

| Project Nam Subject: Location: | 10- | rthern Addition Sidev Yr & 100-Yr Peak Dis ckeye, AZ | | Date; Computed By; Checked By; | 1/19/2015 SAS TAB | PZTEC(©) |
|--------------------------------------|---|--|---------------------------|--------------------------------------|---|--|
| Drainage Ba | asin: DA06 | | | | | |
| | | | | | | |
| | Length | of Longest Flowpath = | 490 feet | | | |
| | | Upper Elevation= | 0.09 miles 879.05 feet | | | |
| | Slone | Lower Elevation= of Longest Flowpath = | 875.25 feet | | | |
| | Siope | Kb = | | | | |
| Tc=11.4L ^{0.5} | ⁰ Кь ^{0.52} Ѕ ^{-0.31} І ^{-0.38} | | | Q=CIA | | |
| Trials | 10-Year Event | | | | C _{10 Subdivision} | |
| Tc (min) | l(in/hr) | Calculated Tc (min) | | | C _{10 Paved} | , |
| 7 | 4.67 | 6.7 | | | | = 3.92 in/hr |
| 8 | 4,42 | 6.9 | | | Area _{Subdivision} | |
| . 9 | 4.17 | 7.0 | | | Area _{Paved} | |
| - 10 | 3.92 | 7.2 | ок | | Total Area | |
| *Minimum T | c = 10 min | | | | | |
| | Denotes information | on that needs to be en | tered. | | 10-Year Storm Event | =cfs |
| Tc=11.4L ^{0.5} | ⁰ К _ь ^{0,52} S ^{-0,31} I ^{-0,38} | · | | Q=CIA | | |
| Trials | 100-Year Event | | | | <u></u> | = 0.60 |
| Tilalo | 100-1ear Lvein | Calculated | | | $C_{100~ m Subdivision}$ $C_{100~ m Paved}$ | |
| To (min) | l(in/hr) | To (min) | | | C ₁₀₀ Composite | Annual Company of the |
| 7 | 7.26 | 5.7 | | | → 100 Composite | |
| 8 | 6.88 | 5.8 | | | Area _{Subdivision} | and the second and th |
| 9 | 6.50 | 5.9 | | | Area _{Paved} | |
| 10 | 6.12 | 6.1 | OK | | Total Area | = 1.71 acres |
| *Minimum T | c = 10 min | | | | | |
| | Denotes information | on that needs to be en | tered. | | 100-Year Storm Event | = 6.9 cfs |
| | , | | | | | |

| Project Name: Subject: Location: | Northern Addition Side 10-Yr & 100-Yr Peak Di Buckeye, AZ | • | Date: Computed By: Checked By: | 1/19/2015 SAS TAB | AZTEC® |
|---|---|--------------------------|--------------------------------------|--|--|
| Drainage Basin: DA0 | 07 | | | | |
| | | | | | |
| | | | | | |
| | Length of Longest Flowpath | = 537 feet 0.10 mile: | ° | | |
| | Upper Elevation | = 877.48 feet | • | | |
| | Lower Elevation Slope of Longest Flowpath | = 21.74 ft/mi | | | |
| | Kb | = 0.0382 | · [| | |
| Tc=11.4L ^{0.50} K _b ^{0.52} S ⁻ | 0.31 _] -0.38 | | Q=CIA | | |
| Trials 10-Year | | | | C _{10 Subdivision} | |
| Tc (min) I(in/ | Calculated 'hr) Tc (min) | | | C _{10 Paved} C _{10 Composite} | Visiting and Committee of the Committee |
| 7 4.6 | | | | | = 3.92 in/hr |
| 8 4.4 | | | | Area _{Subdivision} | District the second |
| 9 4.1 10 3.9 | | ок | | Area _{Paved} Total Area | |
| *Minimum Tc = 10 m | | OK | | rotal Alea | - 1.50 acies |
| Denote | s information that needs to be e | ntered. | | 10-Year Storm Event | =5.0 cfs |
| Tc=11.4L ^{0.50} K _b ^{0.52} S | 0.31[-0.38 | | Q=CIA | | |
| Trials 100-Yea | ar Event | | | G_{100} Subdivision | = 0.60 |
| | Calculated | | | C _{100 Paved} | = 0.95 |
| Tc (min) I(in/ 7 7.2 | | | | C _{100 Composite} | = 0.65 = 6.12 in/hr |
| 8 6.8 | | | | Area _{Subdivision} | PRODUCTOR STREET CONTRACTOR CONTR |
| 9 6.5 | | | | Area _{Paved} | |
| 10 6.1 *Minimum Tc = 10 m | | ок | | Total Area | |
| 20 March 1971 - 1984 - 1984 - 1984 - 1984 - 1984 - 1984 - 1984 - 1984 - 1984 - 1984 - 1984 - 1984 - 1984 - 1984 | | akawa d | | 00 Your Clara Frank | - 7.0 ofc |
|] Denote: | s information that needs to be e | nterea. | | 00-Year Storm Event | = 7.8 cfs |

| Project Name: Subject: Location: | Northern Addition Sidewal 10-Yr & 100-Yr Peak Disch Buckeye, AZ | - | Date: Computed By: Checked By: | 1/19/2015 SAS TAB | AZTEC® |
|---|---|---|--------------------------------------|--|--|
| Drainage Basin: DA0 | 8 | | | | |
| | Length of Longest Flowpath = Upper Elevation= Lower Elevation= Slope of Longest Flowpath = Kb = | 520 feet 0.10 miles 876.88 feet 874.40 feet 25.21 ft/mi 0.0384 | | | |
| Tc=11.4L ^{0,50} K _b ^{0.52} S ^{-9.} | 31 ₁ -0.38 | | Q=CIA | | |
| Trials 10-Year Tc (min) l(in/r) 7 4.6 8 4.4 9 4.1 10 3.9 | Calculated Tc (min) T 8.1 2 8.2 7 8.4 2 8.6 | ок | | C ₁₀ subdivision [*] C ₁₀ Paved [*] C ₁₀ composite [*] l: Area _{Subdivision} [*] Area _{Paved} Total Area: | = 0.95 = 0.65 = 3.92 in/hr = 1.56 acres = 0.26 acres = 1.82 acres |
| Denotes | information that needs to be enter | ea. | | 10-Year Storm Event | = <u>4.6</u> cfs |
| Tc=11.4L ^{0,50} K _b ^{0,52} S ^{-0,} | .31 ₁ -0.38 | | Q=CIA | | |
| Trials 100-Yea Tc (min) (in/r) 7 7.20 8 6.80 9 6.50 10 6.12 *Minimum Tc = 10 mi | Calculated fr) Tc (min) 6 6.8 7.0 7.1 7.1 7.3 | ОК | | C ₁₀₀ subdivision C ₁₀₀ Paved C ₁₀₀ composite I: Area _{Subdivision} Area _{Paved} Total Area: | = 0.95 = 0.65 = 6.12 in/hr = 1.56 acres = 0.26 acres |
| Security commonweal conferences | information that needs to be enter | ed. | 1 | 00-Year Storm Event | = |



Hydraulic Calculations

10-Year Event Full Street Narramore - 1st-2nd (DA01)

Project Description

Friction Method Manning Formula Solve For Normal Depth

Input Data

0.00630 Channel Slope ft∕ft 2.30 ft³/s Discharge

Section Definitions

| Station (ft) | Elevation (ft) |
|--------------|----------------|
| | |
| 0+00 | 100.00 |
| 0+05 | 99.93 |
| 0+05 | 99.43 |
| 0+37 | 99.92 |
| 0+37 | 100.27 |
| 0+42 | 100.35 |

Roughness Segment Definitions

| Start Station En | | ness Coefficient |
|------------------|----------------|------------------|
| (0+00, 100.00) | (0+05, 99.43) | 0.015 |
| (0+05, 99.43) | (0+37, 99.92) | 0.015 |
| (0+37, 99.92) | (0+42, 100.35) | 0.015 |

Options

Current Roughness Weighted Method Pavlovskii's Method Open Channel Weighting Method Pavlovskii's Method Pavlovskii's Method Closed Channel Weighting Method

| Results | | |
|------------------|--------------------|-----|
| Normal Depth | 0.20 | ft |
| Elevation Range | 99.43 to 100.35 ft | |
| Flow Area | 1.35 | ft² |
| Wetted Perimeter | 13.49 | ft |
| Hydraulic Radius | 0.10 | ft |

10-Year Event Full Street Narramore - 1st-2nd (DA01)

| | | | | |
|---------------------|-------------|----------|-------|------|
| Results | | | | |
| Top Width | | 13.32 | ft | |
| Normal Depth | | 0.20 | ft | |
| Critical Depth | | 0.20 | ft | |
| Critical Slope | | 0.00720 | ft/ft | |
| Velocity | | 1.70 | ft/s | |
| Velocity Head | | 0.04 | ft | |
| Specific Energy | | 0.25 | ft | |
| Froude Number | | 0.94 | | |
| Flow Type | Subcritical | | | |
| GVF Input Data | | | | |
| Downstream Depth | | 0.00 | ft | |
| Length | | 0.00 | ft | |
| Number Of Steps | | 0 | | |
| GVF Output Data | | | | |
| Upstream Depth | | 0.00 | ft | |
| Profile Description | | | | |
| Profile Headloss | | 0.00 | ft | |
| Downstream Velocity | | Infinity | ft/s | |
| Upstream Velocity | | Infinity | ft/s | |
| Normal Depth | | 0.20 | ft | |
| Critical Depth | | 0.20 | ft | |
| Channel Slope | | 0.00630 | ft/ft | |
| Critical Slope | | 0.00720 | ft/ft | |
| | | | | |

| | · · · · · · · · · · · · · · · · · · · | |
|---------------------|---------------------------------------|--|
| Project Description | | |
| Solve For | Spread | |
| Input Data | | |
| Channel Slope | 0.00200 ft/ft | |
| Discharge | 3.10 ft³/s | |
| Gutter Width | 1.50 ft | |
| Gutter Cross Slope | 0.06 ft/ft | |

0.01 ft/ft

1.25 ft/s

0.015

10-Year Event Narramore - 2nd-3rd (DA02)

| Results | | | 001846 183789 |
|-------------------|-------|-----|------------------|
| Spread | 22.04 | ft | |
| Flow Area | 2.48 | ft² | |
| Depth | 0.29 | ft | |
| Gutter Depression | 0.07 | ft | |

Road Cross Slope

Velocity

Roughness Coefficient

| 10-Year Event 3rd Street South of Narramore | | | | | |
|---|--------|---------|-------|--|--|
| Project Description | | | | | |
| Solve For | Spread | | | | |
| Input Data | | | | | |
| Channel Slope | | 0.00250 | ft/ft | | |
| Discharge | | 5.40 | ft³/s | | |
| Gutter Width | | 1.50 | ft | | |
| Gutter Cross Slope | | 0.06 | ft/ft | | |
| Road Cross Slope | | 0.01 | ft/ft | | |
| Roughness Coefficient | | 0.015 | | | |
| Results | | | | | |
| Spread | | 26.17 | ft | | |
| Flow Area | | 3.48 | ft² | | |
| Depth | | 0.33 | ft | | |
| Gutter Depression | | 0.07 | ft | | |

1.55 ft/s

Velocity

10-Year Event Narramore - 3rd-4th (DA03)

| | U-Year Event Warr | amore | 3FU-4LN (DAV3) |
|-----------------------|-------------------|---------|----------------|
| Project Description | | | |
| Solve For | Spread | | |
| Input Data | | | |
| Channel Slope | | 0.00200 | ft/ft |
| Discharge | | 3.30 | ft³/s |
| Gutter Width | | 1.50 | ft |
| Gutter Cross Slope | | 0.06 | ft/ft |
| Road Cross Slope | | 0.01 | ft/ft |
| Roughness Coefficient | | 0.015 | |
| Results | | | |
| Spread | | 22.59 | ft |
| Flow Area | | 2.60 | ft² |
| Depth | | 0.30 | ft |
| Gutter Depression | | 0.07 | ft |
| Velocity | | 1.27 | ft/s |
| | | | |

10-Year Event Nelson - 3rd-4th (DA04)

| | 10-1 ear Event i | <u> </u> | u-+tii (DAU+) | |
|-----------------------|------------------|----------|---------------|--|
| Project Description | | | | |
| Solve For | Spread | | | |
| Input Data | | | | |
| Channel Slope | | 0.00700 | ft/ft | |
| Discharge | | 2.30 | ft³/s | |
| Gutter Width | | 1.50 | ft | |
| Gutter Cross Slope | | 0.06 | ft/ft | |
| Road Cross Slope | | 0.01 | fVft | |
| Roughness Coefficient | | 0.015 | | |
| Results | | | | |
| Spread | | 15.27 | ft | |
| Flow Area | | 1.22 | ft² | |
| Depth | | 0.22 | ft | |
| Gutter Depression | | 0.07 | ft | |
| Velocity | | 1.88 | ft/s | |
| | | | | |

| | 10-Year Event Ea | son - 2nd | d-3rd (DA05) | |
|-----------------------|------------------|-----------|--------------|--|
| Project Description | | | | |
| Solve For | Spread | | | |
| Input Data | | | | |
| Channel Slope | • | 0.00280 | ft/ft | |
| Discharge | | 2.70 | ft³/s | |
| Gutter Width | | 1.50 | ft | |
| Gutter Cross Slope | | 0.06 | ft/ft | |
| Road Cross Slope | | 0.02 | ft/ft | |
| Roughness Coefficient | | 0.015 | | |
| Results | | | | |
| Spread | | 12.70 | ft | |
| Flow Area | | 1.66 | ft² | |
| Depth | | 0.31 | ft | |
| Gutter Depression | | 0.06 | ft | |
| Velocity | | 1.63 | ft/s | |

| | 0-Year Event | Eason - 3rd | i-4ti |
|-----------------------|--------------|-------------|----------------------|
| Project Description | | | |
| Solve For | Spread | | |
| Input Data | | | |
| Channel Slope | | 0.00500 | ft/ft |
| Discharge | | 2.20 | ft³/s |
| Gutter Width | | 1.50 | ft |
| Gutter Cross Slope | | 0.06 | ft/ft |
| Road Cross Slope | | 0.02 | ft/ft |
| Roughness Coefficient | | 0.015 | |
| Results | | | 80 33 63 80 80 80 |
| Spread | | 10.45 | ft |
| Flow Area | | 1.13 | ft² |
| Depth | | 0.27 | ft |
| Gutter Depression | | 0.06 | ft |

1.94 ft/s

Velocity

10-Year Event Edison - 2nd-3rd (DA07)

| | O-1001 Elent E | <u> </u> | a 0.a (21.01) |
|-----------------------|----------------|----------|---------------|
| Project Description | | | |
| Solve For | Spread | | |
| Input Data | | | |
| Channel Slope | | 0.00230 | fVft |
| Discharge | | 2.50 | ft³/s |
| Gutter Width | | 1.50 | ft |
| Gutter Cross Slope | | 0.06 | ft/ft |
| Road Cross Slope | | 0.02 | ft/ft |
| Roughness Coefficient | | 0.015 | |
| Results | | | |
| Spread | | 12.81 | ft |
| Flow Area | | 1.68 | ft² |
| Depth | | 0.31 | ft |
| Gutter Depression | | 0.06 | ft |
| Velocity | | 1.48 | ft/s |

| 10-Year Event Edison - 3rd-4th (DA08) | | | | | |
|---------------------------------------|--------|---------|-------|--|--|
| Project Description | | | | | |
| Solve For | Spread | | | | |
| Input Data | | | | | |
| Channel Slope | | 0.00310 | ft/ft | | |
| Discharge | | 2.30 | ft³/s | | |
| Gutter Width | | 1.50 | ft | | |
| Gutter Cross Slope | | 0.06 | ft/ft | | |
| Road Cross Slope | | 0.02 | ft/ft | | |
| Roughness Coefficient | | 0.015 | | | |
| Results | | | | | |
| Spread | | 11.69 | ft | | |
| Flow Area | | 1.41 | ft² | | |
| Depth | | 0.29 | ft | | |
| Gutter Depression | | 0.06 | ft | | |

1.63 ft/s

Velocity



Sidewalk Plans with Finished Floor Elevations